

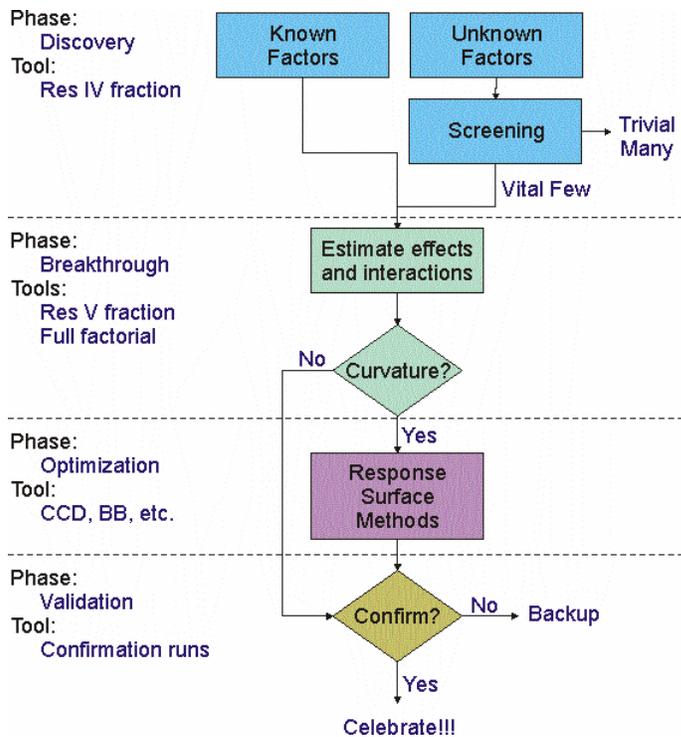
## A STICKY OPTIMIZATION

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Technical professionals in the pressure sensitive adhesives area are highly skilled and educated in tape-making processes. They have often taken course-work in the areas of PSA tape properties, characteristics of tape-making, web handling, coating and converting processes. Subject-matter knowledge is generally abundant. The purpose of this paper is to demonstrate a statistical methodology that builds on subject-matter knowledge to objectively fine-tune both processes and product formulations. The method will be illustrated with a case study where the experimenter was trying to optimize an adhesive to achieve specific test properties.

What methods are currently used for process optimization? How do you find the ideal settings when there are competing criteria? Design of experiments (DOE) is a formalized method of data collection and analysis. Computer technology has turned what used to be a series of tedious mathematical calculations into fairly quick, yet sophisticated, analyses. From these analyses, a subject-matter expert can optimize process settings by making knowledgeable trade-offs in the response criteria. DOE can be used both in laboratory research and out on the manufacturing plant floor.

Researchers and engineers who are unfamiliar with DOE can be overwhelmed by the number of design options. Designed experiments can be run to accomplish many different goals. The right design must be chosen in order to meet the objective of the problem. Figure 1 illustrates how the objective of the design determines the type of design chosen. The discovery phase uses screening designs to identify the primary factors that control the system. These designs are especially helpful to quickly sift through a large number of possible factors, whose true contributions to the system are not understood. Typically, two-level fractional-factorial designs are used in this phase, preferably something called a Resolution IV design<sup>1</sup>. The breakthrough phase uses either full factorial or slightly fractional factorial designs (Resolution V or higher) to positively identify both main effects and interaction effects. At this point, center points may also be added to the design in order to determine if any quadratic effects might be present. The optimization phase is required when at least some of the factors have a curvilinear relationship with some of the responses. It uses response surface designs such as central composite (CCD) and Box-Behnken (BB) designs<sup>2</sup>. Lastly, validation runs finalize the DOE process by confirming the results in a longer-term setting.



**Figure 1.** Strategy of Experimentation

## Case Study

A client manufacturing an adhesive wanted to ensure that the final adhesion properties could be consistently achieved. This entailed identifying optimal processing conditions. Preliminary work determined that there were three key factors that were critical to the manufacturing process. The names of these factors have been removed to protect proprietary information. The engineer responsible for the process decided that he needed to run a designed experiment with the goal of process optimization. This goal meant that a response surface design was in order.

Two standard response surface designs are central composite designs and Box-Behnken designs. This client chose the Box-Behnken design because each of his three factors could be easily set to the three levels required by the design. The total number of runs is 17, which was deemed reasonable by the manufacturing personnel. The design is shown in Table 1. The runs are physically completed in the random run order. Notice that the design includes five center points that are randomly scattered throughout the other runs.

Product samples were made at each of the 17 sets of conditions. The laboratory then measured seven key quality characteristics including some viscosities, tensiles, and subtak and subadhesion properties. This data was entered into a statistical software package that can perform an analysis of variance in order to establish a polynomial prediction equation for each response.

**Table 1.** Box-Behnken design points

Std Order	Run Order	X1	X2	X3
1	15	30	356	12.5
2	5	70	356	12.5
3	1	30	380	12.5
4	8	70	380	12.5
5	16	30	368	5
6	3	70	368	5
7	6	30	368	20
8	14	70	368	20
9	13	50	356	5
10	11	50	380	5
11	12	50	356	20
12	10	50	380	20
13	9	50	368	12.5
14	4	50	368	12.5
15	17	50	368	12.5
16	2	50	368	12.5
17	7	50	368	12.5

### Sample Data Analysis

The analysis of data from a designed experiment is done using a statistical tool called analysis of variance. Table 2 illustrates an example of the analysis of one of the responses in this design – Tensile@0day. Without going into all the details of how this analysis is created, it is more important for an experimenter to understand how to interpret the information presented.

The p-value is the primary column of interest. It quantifies how significant each term is in the polynomial model. A smaller number is better, and as a general rule of thumb, terms are considered statistically significant when their p-value is 0.05 or lower. In this case all but one of these terms is substantially lower than 0.05. You might notice that the AC term is missing. This term had a p-value significantly higher than 0.05, so it was removed from the model.

Lack of fit is another important statistic that shows how well the model fits the data. It is also measured by a p-value, but in this case, it is desirable for the p-value to be higher than 0.10. This indicates that “lack of fit” is not significant, thereby implying that the model fits the data.

In addition to the p-values, the R-squared values given in the lower part of the table are also of interest when a response surface design is run. The adjusted R-squared represents the amount of variation in the data that is explained by the model. The predicted R-squared represents the amount of variation in predictions that is explained by the model. When the objective of the experiment is to optimize, higher R-squared values are important, implying that the polynomial model is a very good predictor of the response. The higher the R-squared values are, the better the polynomial is at either describing the

system or making predictions about the system. For this response, the R-squared values of approximately 98-99% indicate that this polynomial is a very good description of the relationship between these three factors and the Tensile@0day response.

**Table 2.** Analysis of variance for Tensile @ 0day response

**ANOVA for Response Surface Reduced Quadratic Model**

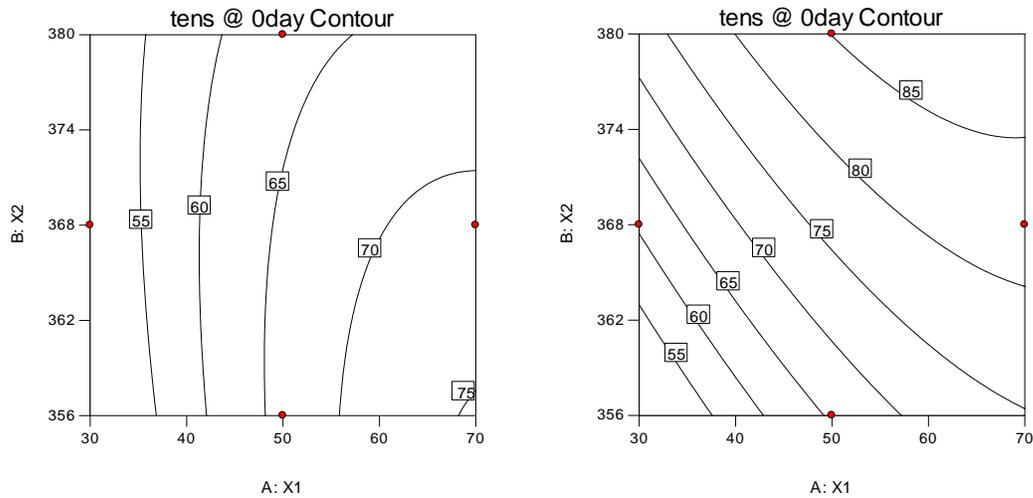
<b>Source</b>	<b>Sum of Squares</b>	<b>df</b>	<b>Mean Square</b>	<b>F Value</b>	<b>p-value Prob &gt; F</b>
<b>Model</b>	1615.57	8	201.95	293.50	< 0.0001
A-X1	933.12	1	933.12	1356.16	< 0.0001
B-X2	128.80	1	128.80	187.19	< 0.0001
C-X3	230.05	1	230.05	334.35	< 0.0001
AB	40.96	1	40.96	59.53	< 0.0001
BC	131.10	1	131.10	190.54	< 0.0001
A <sup>2</sup>	101.40	1	101.40	147.38	< 0.0001
B <sup>2</sup>	4.06	1	4.06	5.91	0.0412
C <sup>2</sup>	34.98	1	34.98	50.84	< 0.0001
<b>Residual</b>	5.50	8	0.69		
<b>Lack of Fit</b>	2.95	4	0.74	1.16	0.4455
<b>Pure Error</b>	2.55	4	0.64		
<b>Cor Total</b>	1621.08	16			
<b>Std. Dev.</b>	0.8295		<b>R-Squared</b>	0.9966	
<b>Mean</b>	69.7118		<b>Adj R-Squared</b>	0.9932	
<b>C.V. %</b>	1.1899		<b>Pred R-Squared</b>	0.9811	
<b>PRESS</b>	30.64		<b>Adeq Precision</b>	58.3012	

**Sample Graphical Analysis**

The statistical analysis should be validated by an examination of residual diagnostics plots. This step is not illustrated here, but should not be over-looked. Typically, the experimenter would confirm that the studentized residuals follow a normal distribution, and that they have a constant variance. Also, the data should be checked to make sure it contains no discrepant values. After the diagnostic validation step is complete, graphical illustrations of the model can be produced as shown by the contour plots in Figure 2.

These contour plots have X1 on the horizontal axis and X2 on the vertical axis, with X3 fixed at a specific level (in this case the low and high levels of 5 and 20.) Tensile@0day predicted contours fill the graphical area. According to the experimenter’s subject matter knowledge, the optimal response value is 65. Notice that on the left-hand graph, there is a contour line labeled “65” that cuts through the middle of the graph area. When X3 is set at its low value of 5, any of the combinations of X1 and X2 settings that fall on that 65

line would be feasible. Now the X3 factor is moved to its high setting of 20 and the right-hand graph shows the line for “65” falling closer to the lower-left corner.



**Figure 2.** Contour plots with X3 set at low level (left) and high level (right)

### Multiple Response Optimization

Typically, the quality of a product is measured by many different quality characteristics. This case study has seven different responses, each of which is modeled with a different polynomial equation. Some models will be linear (containing only terms such as A and B), while others are quadratic (containing squared terms to model non-linearity.)

Accordingly, each will have different contour plots with differing “optimal” factor settings. Working through these graphs by hand for seven different response can be a very time-consuming and inefficient process, as well as prone to mistakes. Statistical software packages typically have a mathematical multiple response optimization routine. This is a method of pulling together all the polynomial models and determining a set of conditions that is a compromise to all the stated goals.

Table 3 shows a summary of all seven responses, the terms that were significant in their models, and summary statistics for each model. Typically, some of the responses will fit to polynomials better than others. In this case, Tensile @ Oday fits almost perfectly, while Subadhesion does not fit as well, but is still adequate.

**Table 3.** Summary of seven response models

<b>Model Term</b>	<b>Visc Init</b>	<b>Visc @50%</b>	<b>Rels @24h</b>	<b>Tens @0day</b>	<b>Tens @3day</b>	<b>Subtak @0day</b>	<b>Subadh @0day</b>
<b>Transform</b>		Log				Log	
<b>A</b>	X	X	X	X	X	X	X
<b>B</b>	X	X	X	X	X	X	
<b>C</b>		X	X	X	X	X	X
<b>AB</b>	X	X	X	X	X	X	
<b>AC</b>		X				X	
<b>BC</b>				X	X		
<b>A<sup>2</sup></b>	X	X	X	X	X	X	
<b>B<sup>2</sup></b>			X	X	X	X	
<b>C<sup>2</sup></b>				X	X		
<b>p-value</b>	<0.0001	0.0007	<0.0001	<0.0001	<0.0001	<0.0001	0.0003
<b>Lack of fit</b>	0.9079	0.5673	0.3197	0.4455	0.1680	0.8156	0.2461
<b>Adj R-sqr</b>	0.9222	0.7880	0.8662	0.9932	0.9704	0.9851	0.6487
<b>Pred R-Sqr</b>	0.8659	0.6027	0.6464	0.9811	0.8471	0.9759	0.5518

After the analysis of each response is complete, these models are used in the numerical optimization routine. This case study uses the optimization criteria in Table 4. The goal is the targeted value, but it is surrounded by an acceptable range that is defined by the low and high values.

**Table 4.** Optimization Criteria

<b>Response</b>	<b>Goal</b>	<b>Low</b>	<b>High</b>
Visc initial	65,000	55,000	90,000
Visc @ 50%	35,000	25,000	40,000
Release @ 24h	30	20	100
Tensile @ 0day	65	60	70
Tensile @ 3day	90	80	100
Subtak @ 0day	300	250	450
Subadh @ 0day	20	15	30

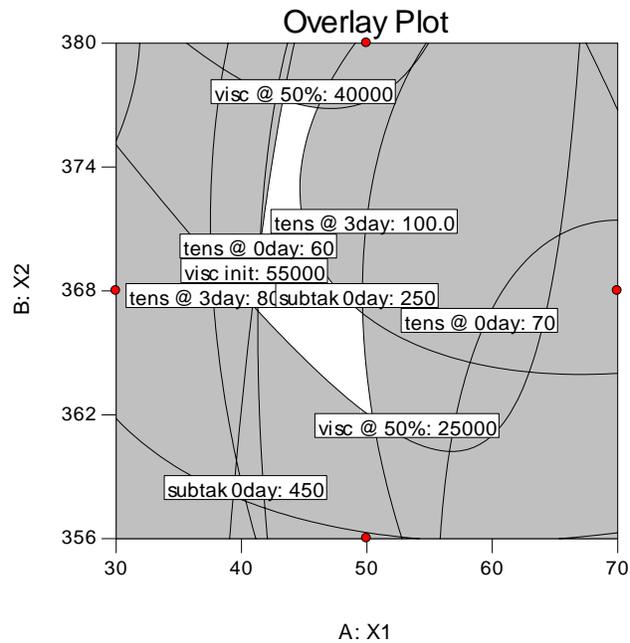
The “sweet spot” in processing conditions that achieves all the goals for this adhesive is shown in Figure 3, which displays factors X1 and X2, with X3 set at its low level of 5.

Design-Expert® Software  
Original Scale  
Overlay Plot

visc init  
visc @ 50%  
relse @ 24h  
tens @ 0day  
tens @ 3day  
subtak 0day  
subadh 0day  
● Design Points

X1 = A: X1  
X2 = B: X2

Actual Factor  
C: X3 = 5.00



**Figure 3.** Multiple response optimization sweet spot

The client may have stumbled upon this set of operating conditions by chance, but it is unlikely that they would have had a clear picture of which responses define this region. It turns out that the left side of the operating window is defined by the initial viscosity limit of 55,000. The bottom is defined by the viscosity@50%, and the right side is defined by both the subtak@0day and the tensile@3day. If the limits of any of these can be expanded, then the operating region will open up. This is a critical gain in process understanding, because it also indicates that the other responses do not control the operating conditions.

## Summary

Design of experiments (DOE) can be a challenge to implement because it differs from traditional one-factor-at-a-time experimentation. Old habits don't necessarily fit into the "DOE way" of doing things. DOE adds tremendous efficiency to understanding how processes work. It allows complex processes to be broken down so that they can be understood as a group of interacting factors.

This was simply one illustration of the use of design of experiments. Two-level factorial DOE can be used to identify which variables in a process are critical to control. Mixture designs are used to optimize a chemical formulation to meet specific criteria. Robust design helps find factor settings that make a product or process robust to variations in uncontrollable variables.

Technical professionals will find many ways to apply design of experiments. It just takes a little education and a bit of practice to discover that experimentation can be done on a whole new level.

### **References**

1. Anderson, M. and Whitcomb, P., 2000, *DOE Simplified, Practical Tools for Effective Experimentation*, Productivity, Inc.
2. Anderson, M. and Whitcomb, P., 2004, *RSM Simplified, Optimizing Processes Using Response Surface Methods for Design of Experiments*, Productivity Press.
3. Montgomery, D. C., 2001, *Design and Analysis of Experiments*, John Wiley & Sons.
4. Helseth, et. al., 2005, Design-Expert v7, Stat-Ease, Inc, <http://www.statease.com>, 612-378-9449.

## Appendix. Table of Raw Data

Std	Run	Factor 1 A:X1	Factor 2 B:X2	Factor 3 C:X3	Response 1 visc init cp	Response 2 visc @ 50% cp	Response 3 relse @ 24h grams	Response 4 tens @ 0day psi	Response 5 tens @ 3day psi	Response 6 subtak 0day oz	Response 7 subadh 0day oz
1	15	30	356	12.5	25500	3150	40	49.4	67	302	15
2	5	70	356	12.5	75000	27500	30	78.4	130	167	13
3	1	30	380	12.5	30000	13500	125	63.9	85.2	212	24
4	8	70	380	12.5	55500	29400	75	80.1	130	61	12
5	16	30	368	5	26500	16900	90	49.8	65.6	379	26
6	7	70	368	5	67000	15300	60	71.1	112.6	200	17
7	6	30	368	20	25500	3800	100	61.7	86.4	98	14
8	14	70	368	20	61500	21900	85	81.6	142	27	4
9	13	50	356	5	82000	32300	20	66.6	92.9	496	23
10	11	50	380	5	58000	40200	65	63.1	98.5	252	22
11	12	50	356	20	76750	8300	60	65.4	102.5	74	17
12	10	50	380	20	57000	28800	90	84.8	139.1	45	10
13	9	50	368	12.5	63750	20300	80	73.5	122.7	93	18
14	4	50	368	12.5	75000	11100	65	72.9	120.6	87	23
15	17	50	368	12.5	67000	18500	75	74.9	116.8	105	20
16	2	50	368	12.5	58000	25600	70	73.5	120.1	117	17
17	3	50	368	12.5	74000	25300	85	74.4	115.7	97	22