

### **Practical DOE – "Tricks of the Trade"**

Presentation is posted at <a href="https://www.statease.com/webinar.html">www.statease.com/webinar.html</a>

**There are many attendees today!** To avoid disrupting the Voice over Internet Protocol (VoIP) system, I will <u>mute</u> all. Please email Questions to me which I answer after the presentation.

-- Pat



Presented by Pat Whitcomb, Founder Stat-Ease, Inc., Minneapolis, MN pat@statease.com

#### Practical DOE "Tricks of the Trade"



- Using standard error to constrain optimization
- ➤ Employing C<sub>pk</sub> (or P<sub>pk</sub>) to optimize your DOE
- Combining categoric factors
- A Couple of Case Studies
  - The Loose Collet
  - A Case to Test Your Metal

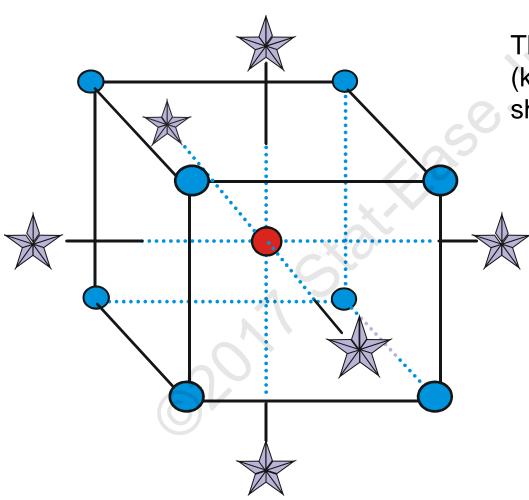
### Practical DOE "Tricks of the Trade"



- Using standard error to constrain optimization Expand your search without sacrificing precision. 5 times the volume with no loss in precision!
- $\triangleright$  Employing  $C_{pk}$  (or  $P_{pk}$ ) to optimize your DOE
- Combining categoric factors
- A Couple of Case Studies
  - The Loose Collet
  - A Case to Test Your Metal

### Four Factor CCD — Case Study #1 alpha = 2.0 (rotatable and spherical)





There are four factors (k=4), but picture only shows three factors.

### Four Factor CCD — Case Study #1 Standard Error of the Mean



Prediction standard error of the expected value:

$$PV(x_0) = var(\hat{\overline{y}}_0) = (x_0^T (X^T X)^{-1} x_0) s^2$$

$$StdErr(x_0) = s_{\hat{y}_0} = \sqrt{PV(x_0)}$$

- x<sub>0</sub> the location in the design space (i.e. the x coordinates for all model terms).
- X the experimental design (i.e. where the runs are in the design space).

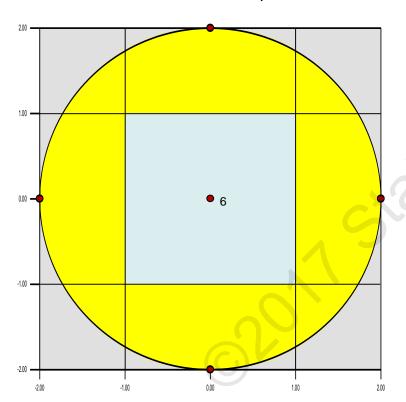
In this four factor CCD, the factorial and axial points have:

$$StdErr = 3.43744$$

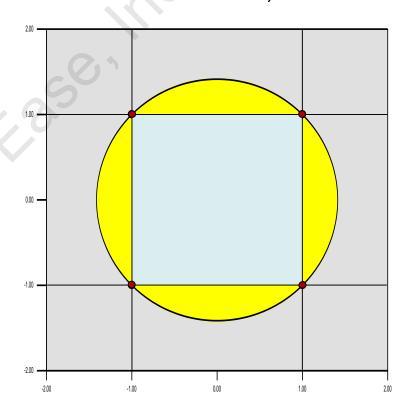
### Four Factor CCD — Case Study #1 alpha = 2.0 (rotatable and spherical)



Slice at: C = 0, D = 0



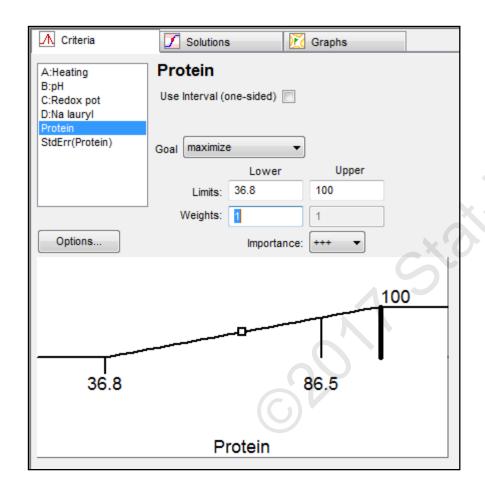
Slice at: C = +1, D = +1

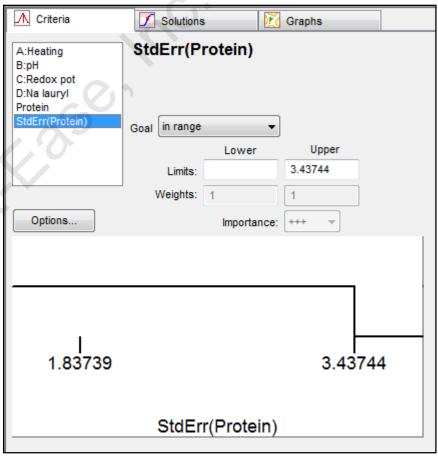


Yellow border at StdErr = 3.43744

### Four Factor CCD — Case Study #1 Maximize Protein with StdErr ≤ 3.43744

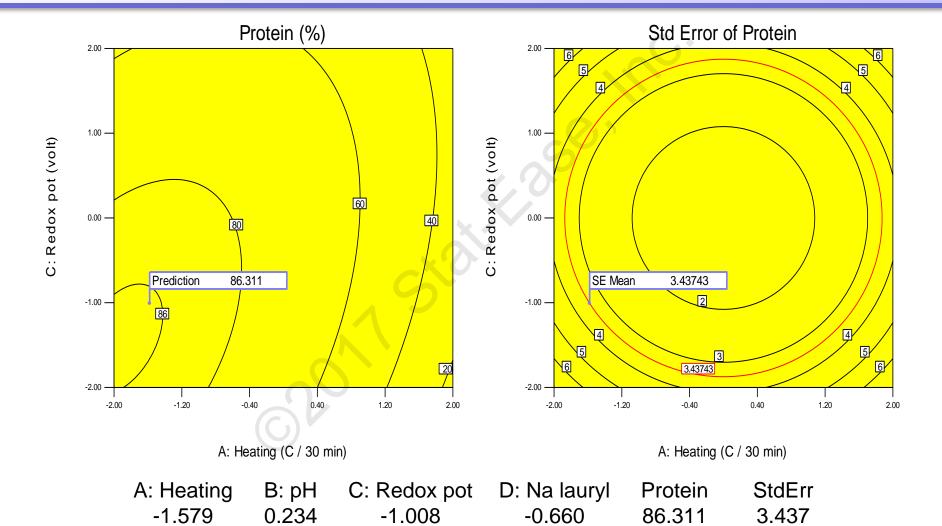






### Four Factor CCD — Case Study #1 Maximize Protein with StdErr ≤ 3.43744





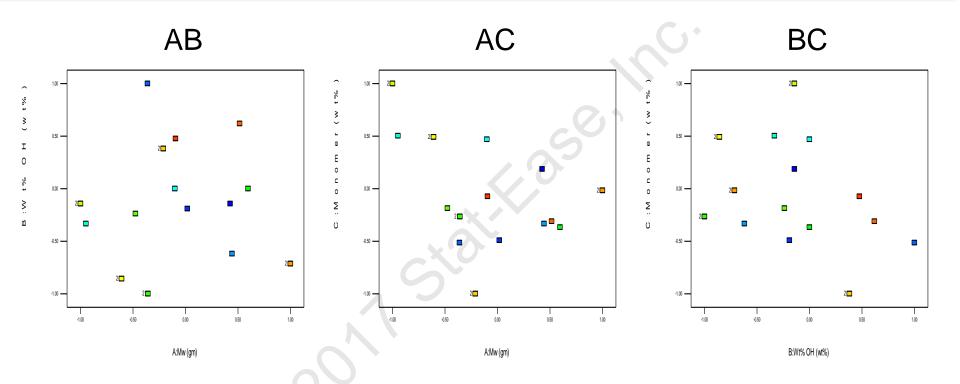
### Four Factor CCD – Case Study #1 Maximize Protein



| A            | В        | C             | D            | y             |          |
|--------------|----------|---------------|--------------|---------------|----------|
| Heating      | рН       | Redox pot     | Na lauryl    | Protein       | StdErr   |
| Factor range | e ±1.00  | cube (too     | restrictive) | (max SE =     | 3.43744) |
| -1.000       | -0.157   | -0.870        | -0.999       | 84.696        | 2.595    |
|              |          |               |              |               |          |
| Factor range | e ±2.00  | cube (to      | o liberal)   | (max SE =     | 13.3764) |
| -2.000       | 0.636    | -2.000        | -2.000       | 89.644        | 10.321   |
|              |          |               |              |               |          |
| SE ≤ 3.4374  | 4 spher  | e (ju         | ıst right)   | (max SE =     | 3.43744) |
| -1.579       | 0.234    | -1.008        | -0.660       | 86.311        | 3.437    |
| ir           | ncreases | s volume of s | earch by 393 | 3% over ±1 cu | ube      |

### Historical Data — Case Study #2 Not Space Filling for Cube or Sphere

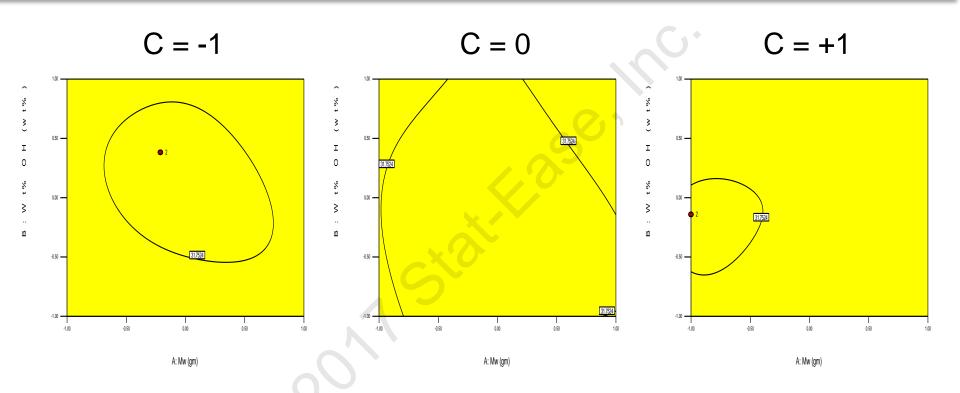




Points projected in two-dimensional planes.

### Historical Data — Case Study #2 Limit Search to StdErr ≤ 31.7524

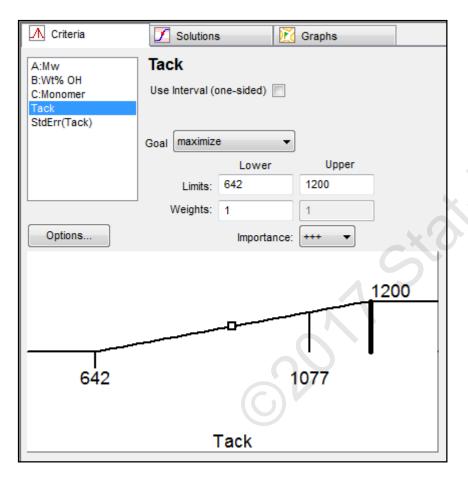


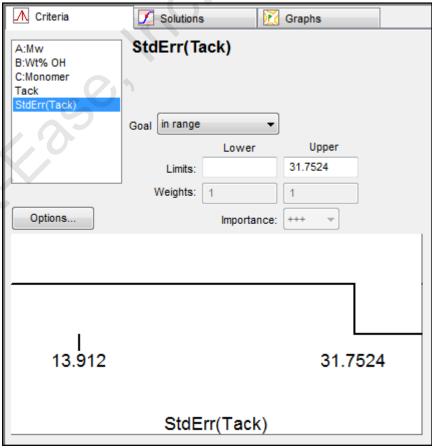


Highest Standard Error at a design point = 31.7524

### Historical Data — Case Study #2 Maximize Tack with StdErr ≤ 31.7524







### Historical Data — Case Study #2 Maximum Tack with StdErr ≤ 31.7524



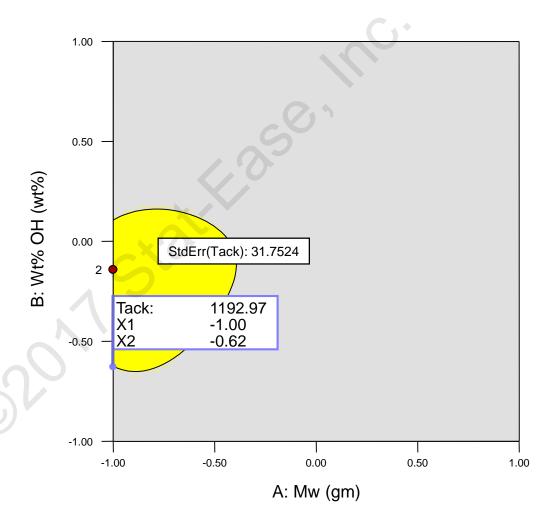
Design-Expert® Software Factor Coding: Coded Overlay Plot

Tack
StdErr(Tack)

Design Points

X1 = A: Mw X2 = B: Wt% OH

Coded Factor C: Monomer = 1.000



# Conclusions: Using Standard Error to Constrain Optimization



#### Advantages:

- Defines a search area that matches design properties:
  - Spheres for rotatable CCDs.
  - Cubes for face centered CCDs.
  - Irregular shapes for optimal designs and historical data.
- Modifies search area for reduced models and missing data.

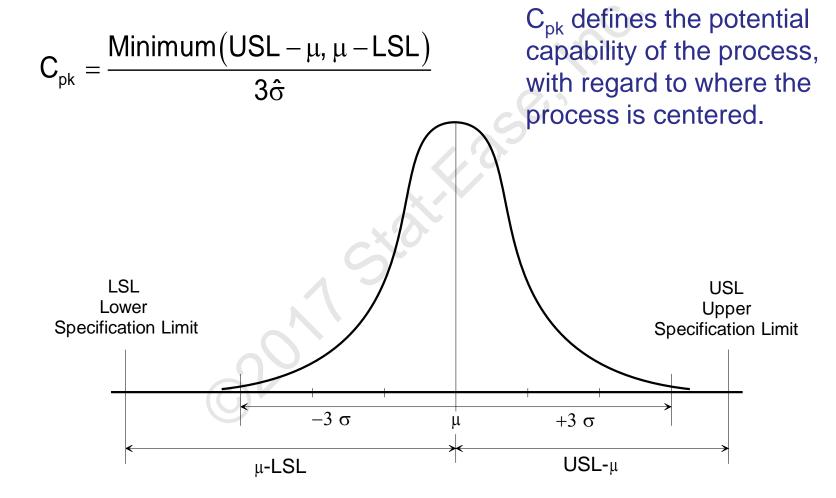
#### Practical DOE "Tricks of the Trade"



- Using standard error to constrain optimization
- **▶** Employing C<sub>pk</sub> (or P<sub>pk</sub>) to optimize your DOE Incorporate specifications in your optimization.
- Combining categoric factors
- A Couple of Case Studies
  - The Loose Collet
  - A Case to Test Your Metal

# Process Capability Refresher C<sub>pk</sub> statistic





# Process Capability Refresher P<sub>pk</sub> statistic



P<sub>pk</sub> statistic is used to determine how "in control" the process has been over time.

$$Z_{upper} = \frac{USL - \overline{\overline{Y}}}{3\hat{\sigma}_s}, \quad Z_{lower} = \frac{\overline{\overline{Y}} - LSL}{3\hat{\sigma}_s}$$

$$P_{pk} = minimum(Z_{upper}, Z_{lower})$$
  $P_{pk}$  allows for variation from a centered process.

 $\hat{\sigma}_s$  is calculated from data gathered over time to capture long term variation.

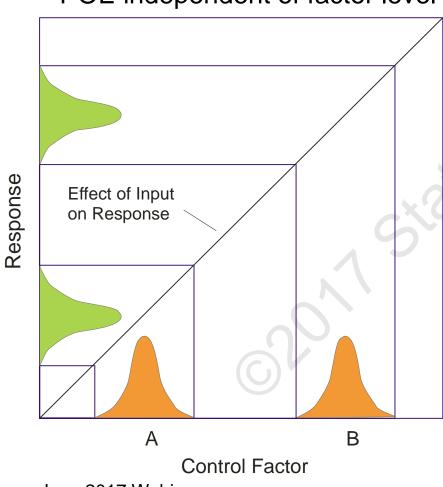
The difference between  $C_{pk}$  and  $P_{pk}$  is the estimate of sigma:

- C<sub>pk</sub> uses a short term estimate of sigma
- P<sub>pk</sub> uses a long term estimate of sigma

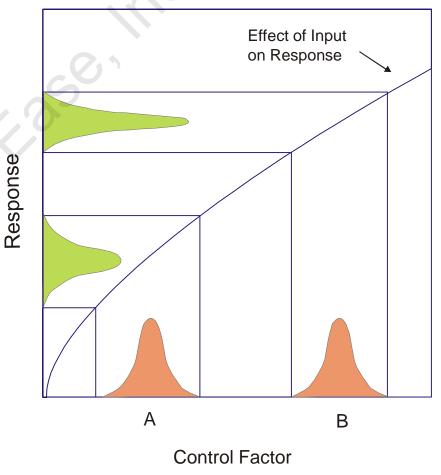
### Propagation of Error Tool to Improve C<sub>pk</sub> & P<sub>pk</sub>



POE independent of factor level



#### POE dependent on factor level



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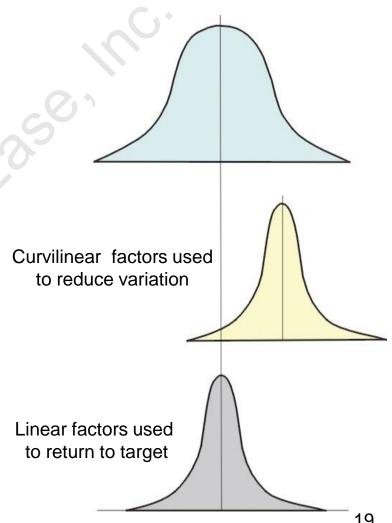
18

### Propagation of Error **Achieve Target with Less Variation**



To illustrate the theory, the control factors were used in two steps: first to decrease variation and second to move back on target.

In practice, numerical optimization can be used to simultaneously obtain all the goals.



### Propagation of Error



### Goal: Minimize Propagated Error (POE)

#### First order:

$$\sigma^{2}_{\hat{Y}} = \sum_{i} \left( \frac{\partial f}{\partial x_{i}} \right)^{2} \sigma^{2}_{x_{i}} + \sigma^{2}_{e}$$

$$\hat{y} = f(x_{1}, ..., x_{k})$$



#### **Second order:**

$$\sigma^2_{~\hat{\gamma}} = \sum_{i=1}^k \Biggl(\frac{\partial f}{\partial x_i}\Biggr)^2 \, \sigma_{ii}^2 + \frac{1}{2} \sum_{i=1}^k \Biggl(\frac{\partial^2 f}{\partial x_i^2}\Biggr)^2 \, \sigma_{ii}^4 + \sum_{i < j}^k \Biggl(\frac{\partial^2 f}{\partial x_i \partial x_j}\Biggr)^2 \, \sigma_{ii}^2 \sigma_{jj}^2 + \sigma_e^2$$

$$\hat{y} = f(x_1, ..., x_k) + \frac{1}{2} \sum_{i=1}^{k} \left( \frac{\partial^2 f}{\partial x_i^2} \right) \sigma_{ii}^2$$

$$\sigma_{e}^{2}=\text{MS}_{\text{residual}}$$
 from the ANOVA and POE  $=\sqrt{\sigma_{~\hat{\gamma}}^{2}}$ 

# Process Capability Refresher C<sub>pk</sub> versus P<sub>pk</sub> statistic



#### The difference between $C_{pk}$ and $P_{pk}$ is the estimate of sigma:

- C<sub>pk</sub> uses a **short** term estimate of sigma
- P<sub>pk</sub> uses a **long** term estimate of sigma

### **Design of Experiments (DOE):**

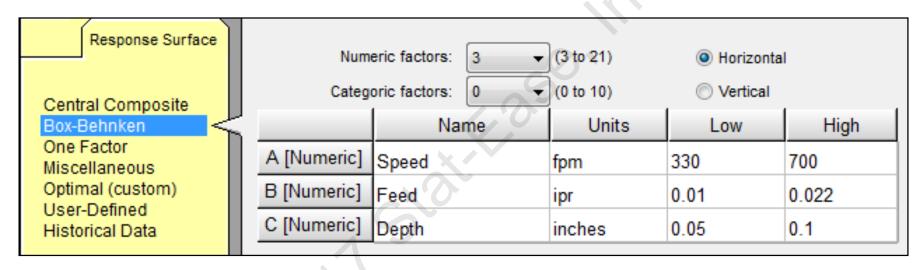
- The residual MSE  $(\sigma_e^2)$  estimates short variation  $(C_{pk})$
- Propagation of error estimates long term variation (P<sub>pk</sub> like)

$$\sigma^2_{\ \hat{\boldsymbol{Y}}} = \sum_{i=1}^k \left(\frac{\partial f}{\partial \boldsymbol{x}_i}\right)^2 \sigma_{ii}^2 + \frac{1}{2} \sum_{i=1}^k \left(\frac{\partial^2 f}{\partial \boldsymbol{x}_i^2}\right)^2 \sigma_{ii}^4 + \sum_{i < j}^k \left(\frac{\partial^2 f}{\partial \boldsymbol{x}_i \partial \boldsymbol{x}_j}\right)^2 \sigma_{ii}^2 \sigma_{jj}^2 + \sigma_e^2$$

### Employing $C_{pk}$ (or $P_{pk}$ ) to optimize your DOE Lathe Case Study



The experimenters run a three factor Box-Behnken design:



The key response is delta, i.e. the deviation of the finished part's dimension from its nominal value. Delta is measured in mils, 1 mil = 0.001 inches.

## Employing $C_{pk}$ (or $P_{pk}$ ) to optimize your DOE Lathe Case Study



| ANOVA for        | ANOVA for Response Surface Reduced Quadratic model             |               |              |        |          |  |  |  |
|------------------|--|---------------|--------------|--------|----------|--|--|--|
| Analysis of vari | Analysis of variance table [Partial sum of squares - Type III] |               |              |        |          |  |  |  |
|                  | Sum of   |               | Mean         | F      | p-value  |  |  |  |
| Source           | Squares  | df            | Square       | Value  | Prob > F |  |  |  |
| Model            | 1.36   | 7             | 0.19         | 42.65  | < 0.0001 |  |  |  |
| A-Speed          | 0.037  | 1             | 0.037        | 8.17   | 0.0189   |  |  |  |
| B-Feed           | 0.15   | 1             | 0.15         | 32.42  | 0.0003   |  |  |  |
| C-Depth          | 0.35   | 1             | 0.35         | 77.80  | < 0.0001 |  |  |  |
| AB               | 0.27   | 1             | 0.27         | 59.70  | < 0.0001 |  |  |  |
| AC               | 0.24   | 1             | 0.24         | 53.21  | < 0.0001 |  |  |  |
| A2               | 0.025  | 1             | 0.025        | 5.52   | 0.0434   |  |  |  |
| C <sup>2</sup>   | 0.27   | 1             | 0.27         | 59.53  | < 0.0001 |  |  |  |
| Residual         | 0.041  | 9             | 4.558E-003   |        |          |  |  |  |
| Lack of Fit      | 0.019  | 5             | 3.740E-003   | 0.67   | 0.6689   |  |  |  |
| Pure Error       | 0.022  | 4             | 5.582E-003   |        |          |  |  |  |
| Cor Total        | 1.40   | 16            |              |        |          |  |  |  |
| Std. Dev.        | 0.068  | R             | -Squared     | 0.9707 |          |  |  |  |
| Mean             | -3.535E-003  | Α             | dj R-Squared | 0.9480 |          |  |  |  |
| C.V. %           | 1909.78  | Pred R-Square |              | 0.8906 |          |  |  |  |
| PRESS            | 0.15   | Α             | deq Precisio | 20.957 |          |  |  |  |

### Employing $C_{pk}$ (or $P_{pk}$ ) to optimize your DOE Lathe Case Study

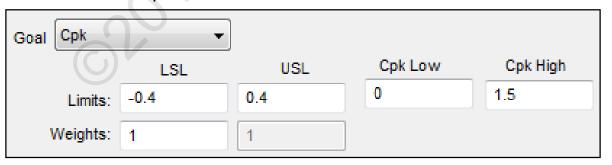


#### Variation of Inputs:

| Variable  | Std Dev: $\widehat{\sigma}_{ii}$ |
|-----------|----------------------------------|
| A – Speed | 5 fpm                            |
| B – Feed  | 0.00175 ipr                      |
| C – Depth | 0.0125 inches                    |

Specifications: Delta =  $0.000 \pm 0.400$ 

Goal is to maximize P<sub>pk</sub>:



### Employing C<sub>pk</sub> (or P<sub>pk</sub>) to optimize your DOE Lathe Case Study



| Factor      | Name      | Level      | Low Level | High Level | Std. Dev.  | Coding     |             |            |             |      |
|-------------|-----------|------------|-----------|------------|------------|------------|-------------|------------|-------------|------|
| A           | Speed     | 8.187E-003 | -1.00     | 1.00       | 5.00       | Coded      |             |            |             |      |
| В           | Feed      | 1.00       | -1.00     | 1.00       | 1.750E-003 | Coded      |             |            |             |      |
| С           | Depth     | -0.41      | -1.00     | 1.00       | 0.013      | Coded      |             |            |             |      |
|             | Predicted | Predicted  |           |            |            | CI for     | Mean        | 99% of     | Population  |      |
| Response    | Mean      | Median1    | Observed  | Std Dev    | SE Mean    | 95% CI low | 95% CI high | 95% TI low | 95% TI high | Cpk  |
| delta       | -0.0634   | -0.0634    | -         | 0.0675     | 0.0354     | -0.144     | 0.0167      | -0.414     | 0.288       | 1.66 |
| delta (POE) | 2.02E-008 | 2.02E-008  | -         | 0.12       | 0.0629     | -0.142     | 0.142       | -0.623     | 0.623       | 1.11 |

delta:

 $C_{pk} = 1.66$   $C_{pk} = 1.11$  (more like  $P_{pk}$ ) delta (POE):

# Conclusions: Employing $C_{pk}$ (or $P_{pk}$ ) to optimize your DOE



#### Advantages:

- Brings specifications into the optimization.
- Can use POE to better represent long term variability.
- In multiple response optimization the various process capabilities can be weighted by importance of response.
- Can explore what if questions, e.g. what if there was better control of various factors; e.g. compare C<sub>pk</sub> without POE to C<sub>pk</sub> with POE (P<sub>pk</sub>).

### Practical DOE "Tricks of the Trade"



- Using standard error to constrain optimization
- Employing C<sub>pk</sub> (or P<sub>pk</sub>) to optimize your DOE
- Combining categoric factors Reduce redundancy and number of runs.
- A Couple of Case Studies
  - The Loose Collet
  - A Case to Test Your Metal

### Combining Categoric Factors CWA detection Case Study



Goal: Prove effectiveness of a remote detection system for a chemical-warfare agent (CWA).

#### Factors and levels:

A. CWA (Threshold, Objective)

B. Interferent (None, Burning diesel, Burning plastic)

C. Time (Day, Night)

D. Distance (1 km, 3 km, 5 km)

E. Environment (Desert, Tropical, Arctic, Urban, Forest)

F. Season (Summer, Winter)

G. Temperature (High, Low)

H. Humidity (High, Low)

## Combining Categoric Factors CWA detection Case Study



Looking at the last four factors, there are too many combinations (40) and not all of these combinations are meaningful:

E. Environment (Desert, Tropical, Arctic, Urban, Forest)

F. Season (Summer, Winter)

G. Temperature (High, Low)

H. Humidity (High, Low)

Not meaningful: Tropical with low temperature and low humidity

Arctic with high temperature and high humidity

Solution is to combine these four categorical factors into one.

## Combining Categoric Factors CWA detection Case Study



#### The eight most meaningful combinations:

| Background    | Temperature | Humidity |  |
|---------------|-------------|----------|--|
| Desert Winter | Low         | Low      |  |
| Desert Summer | High        | Low      |  |
| Tropical      | High        | High     |  |
| Arctic        | Low         | Low      |  |
| Urban Winter  | Low         | Low      |  |
| Urban Summer  | High        | High     |  |
| Forest Winter | Low         | Low      |  |
| Forest Summer | High        | High     |  |

# Conclusions: Combining Categoric Factors



#### Advantages:

- Number of runs reduced.
  - Runs reduced by 80% (1,440 to 288) for CWA.
- All the combinations can be run and result in meaningful results.
- Can fit a full model.
   Preventing meaningless (or impossible) runs that result in missing data thereby creating an aliased model.

#### Practical DOE "Tricks of the Trade"



- Using standard error to constrain optimization
- Employing C<sub>pk</sub> (or P<sub>pk</sub>) to optimize your DOE
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- A Couple of Case Studies
  - The Loose Collet
     Diagnostics plus subject matter knowledge save the day.
  - A Case to Test Your Metal

## The Loose Collet \* Background (page 1 of 2)





- 1. A computer controlled lathe feeds in bar stock, cuts it, machines the surface and releases a part. The collet holds the part in place as it is being machined. The operator programs the speed (rate of spin) and feed (depth of cut). The operator hand tightens the collet.
- 2. The response is surface finish, measured on the same one inch section of each part. The higher the reading the rougher the surface. Low readings (a smooth surface) are desirable.

<sup>\*</sup> William H. Collins and Carol B. Collins, Quality Engineering, Vol. 6, No.4, 1994, p. 547.

## The Loose Collet Background (page 1 of 2)





3. The factors studied are:

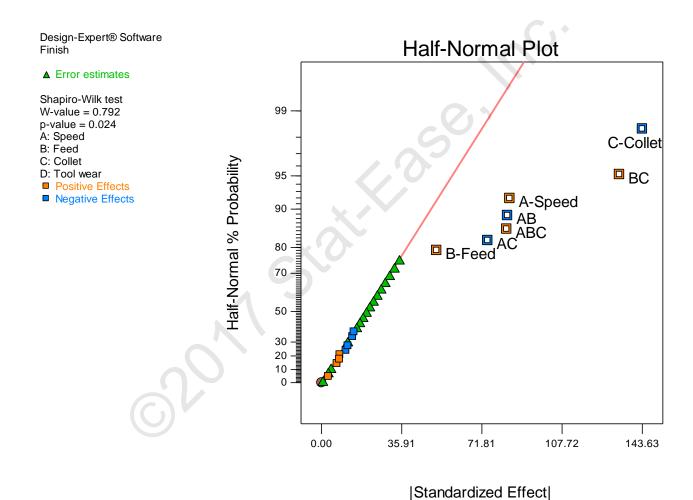
|          | Factor    | -1    | +1              | Units  |
|----------|-----------|-------|-----------------|--------|
| A Speed  |           | 2500  | 4500            | rpm    |
| B Feed   |           | 0.003 | 0.009           | in/rev |
| C Collet |           | Loose | Tight           |        |
| D        | Tool wear | New   | after 250 parts |        |

- 4. The design run was a 2<sup>4</sup> replicated factorial.
- 5. Determine what is causing rough surface?

## The Loose Collet Analysis Replicated 24







### The Loose Collet Analysis Replicated 2<sup>4</sup>





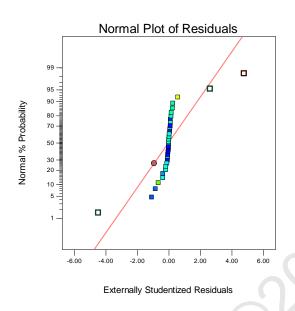
| y | Transform  | Effects    | F <del>+</del> | ANOVA         | Diagnost | tics 🔼 N |  |  |  |  |
|---|--|------------|----------------|---------------|----------|----------|--|--|--|--|
|   |  |            |                |               |          |          |  |  |  |  |
|   | ANOVA for selected factorial model                             |            |                |               |          |          |  |  |  |  |
|   | Analysis of variance table [Partial sum of squares - Type III] |            |                |               |          |          |  |  |  |  |
|   |  | Sum of     |                | Mean          | F        | p-value  |  |  |  |  |
|   | Source   | Squares    | df             | Square        | Value    | Prob > F |  |  |  |  |
|   | Model  | 5.400E+005 | 7              | 77140.36      | 15.32    | < 0.0001 |  |  |  |  |
|   | A-Speed  | 56784.50   | 1              | 56784.50      | 11.28    | 0.0026   |  |  |  |  |
|   | B-Feed   | 21218.00   | 1              | 21218.00      | 4.21     | 0.0511   |  |  |  |  |
|   | C-Collet   | 1.650E+005 | 1              | 1.650E+005    | 32.78    | < 0.0001 |  |  |  |  |
|   | AB   | 55444.50   | 1              | 55444.50      | 11.01    | 0.0029   |  |  |  |  |
|   | AC   | 44253.13   | 0 1            | 44253.13      | 8.79     | 0.0067   |  |  |  |  |
|   | BC   | 1.423E+005 | 1              | 1.423E+005    | 28.27    | < 0.0001 |  |  |  |  |
|   | ABC  | 54946.13   | 1              | 54946.13      | 10.91    | 0.0030   |  |  |  |  |
|   | Residual   | 1.208E+005 | 24             | 5034.38       |          |          |  |  |  |  |
|   | Lack of Fit  | 6763.00    | 8              | 845.38        | 0.12     | 0.9976   |  |  |  |  |
|   | Pure Error   | 1.141E+005 | 16             | 7128.88       |          |          |  |  |  |  |
|   | Cor Total  | 6.608E+005 | 31             |               |          |          |  |  |  |  |
|   | SV   |            |                |               |          |          |  |  |  |  |
|   | Std. Dev.  | 70.95      |                | R-Squared     | 0.8172   |          |  |  |  |  |
|   | Mean   | 203.63     |                | Adj R-Squared | 0.7638   |          |  |  |  |  |
|   | C.V. %   | 34.85      |                | Pred R-Square | 0.6749   |          |  |  |  |  |
|   | PRESS  | 2.148E+005 |                | Adeq Precisio | 12.529   |          |  |  |  |  |

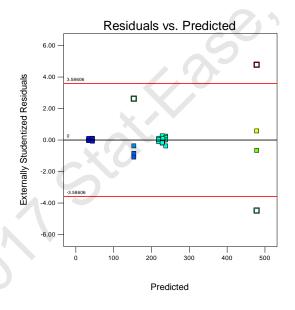
## The Loose Collet Diagnostic Plots Replicated 24

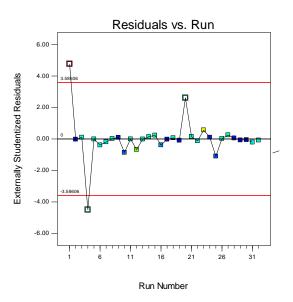




## Residual Plots (runs 1, 4 & 20 are highlighted)







## The Loose Collet Raw Data





#### The residuals from runs 1, 4 and 20 seem unusually large:

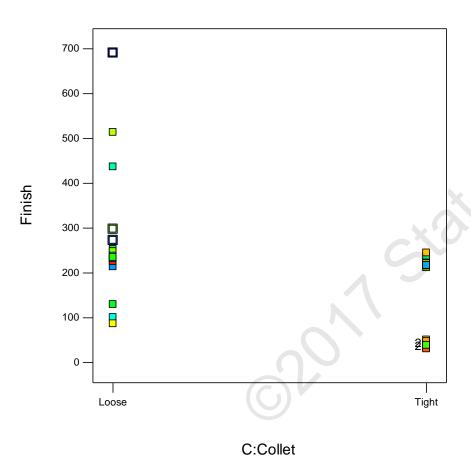
|     |     | Factor  | Factor | Factor   | Factor      | Response |  |  |
|-----|-----|---------|--------|----------|-------------|----------|--|--|
| Std | Run | A:Speed | B:Feed | C:Collet | D:Tool wear | Finish   |  |  |
|     |     | rpm     | in/rev |          | (7)         |          |  |  |
| 1   | 10  | 2500    | 0.003  | Loose    | New         | 101      |  |  |
| 2   | 16  | 2500    | 0.003  | Loose    | New         | 130      |  |  |
| 3   | 4   | 4500    | 0.003  | Loose    | New         | 273      |  |  |
| 4   | 1   | 4500    | 0.003  | Loose    | New         | 691      |  |  |
| 5   | 15  | 2500    | 0.009  | Loose    | New         | 253      |  |  |
| •   |     |         |        |          |             |          |  |  |
| 16  | 27  | 4500    | 0.009  | Tight    | New         | 245      |  |  |
| 17  | 20  | 2500    | 0.003  | Loose    | After 250   | 298      |  |  |
| 18  | 25  | 2500    | 0.003  | Loose    | After 250   | 87       |  |  |
|     |     |         | •      |          |             |          |  |  |
| 31  | 31  | 4500    | 0.009  | Tight    | After 250   | 216      |  |  |
| 32  | 7   | 4500    | 0.009  | Tight    | After 250   | 217      |  |  |
|     |     |         |        |          |             |          |  |  |

These three runs occur when at slow feed and a loose collet. When measuring the surface finish, it was noted that this treatment combination produced an unusual finish. The surface profile looked like a sine wave. The problem is clear; the bar oscillated and caused an uneven cut pattern.

## The Loose Collet Graph Columns







#### What we've learned so far:

- A loose collet is consistently bad.
- Never use a loose collet in production.

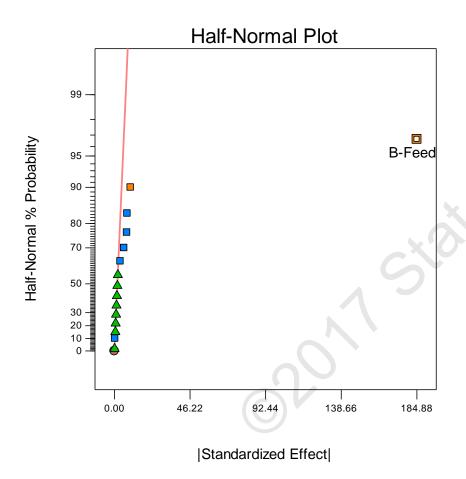
#### Next steps:

- Ignore loose collet data.
- Reanalyze the remaining data (a replicated 2<sup>3</sup> factorial).

## The Loose Collet Analysis w/o Loose Collet







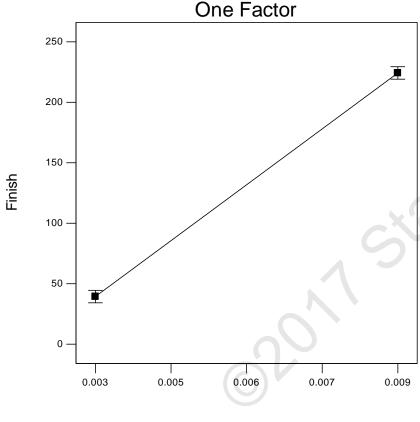
| yλ | Transform  | Effects    |        | ANOVA     | Diagno       | ostics <a> <a> <a> <a> <a> <a> <a> <a> <a> <a></a></a></a></a></a></a></a></a></a></a> |  |  |  |  |
|----|--|------------|--------|-----------|--------------|--|--|--|--|--|
|    |  |            |        |           |              |  |  |  |  |  |
| R  | esponse  | 1          | Finish |           |              |  |  |  |  |  |
|    | These rows were ignored for this analysis.                     |            |        |           |              |  |  |  |  |  |
|    | 10, 16, 4, 1, 15, 6, 13, 32, 20, 25, 23, 12, 21, 11, 8, 18     |            |        |           |              |  |  |  |  |  |
|    |  |            |        |           |              |  |  |  |  |  |
|    | ANOVA for selected factorial model                             |            |        |           |              |  |  |  |  |  |
| A  | Analysis of variance table [Partial sum of squares - Type III] |            |        |           |              |  |  |  |  |  |
|    |  | Sum of     |        | Me        | ean F        | p-value  |  |  |  |  |
| S  | ource  | Squares    | d      | f Squa    | are Value    | Prob > F   |  |  |  |  |
| M  | lodel  | 1.367E+005 | 9      | 1 1.367E+ | 005 1479.86  | < 0.0001   |  |  |  |  |
|    | B-Feed   | 1.367E+005 |        | 1 1.367E+ | 005 1479.86  | < 0.0001   |  |  |  |  |
| R  | esidual  | 1293.37    | 1      | 4 92      | 2.38         |  |  |  |  |  |
|    | Lack of Fit  | 1061.87    | 19     | 6 176     | 6.12         | 0.0113   |  |  |  |  |
|    | Pure Error   | 231.50     | 1      | 8 28      | 3.94         |  |  |  |  |  |
| c  | or Total   | 1.380E+005 | 1      | 5         |              |  |  |  |  |  |
|    |  |            |        |           |              |  |  |  |  |  |
| S  | td. Dev.   | 9.61       |        | R-Squared | 0.9906       | ĺ  |  |  |  |  |
| M  | lean   | 131.81     |        | Adj R-Squ | arec 0.9900  |  |  |  |  |  |
| c  | .V. %  | 7.29       |        | Pred R-Sq | uare 0.9878  |  |  |  |  |  |
| P  | RESS   | 1689.31    |        | Adeq Prec | cisio 54.403 |  |  |  |  |  |

### The Loose Collet Analysis w/o Loose Collet





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B: Feed (in/rev)

#### Take Away:

- Feed (depth of cut) is the only factor that affects surface finish when you use a tight collet!
- A simple solution that could have been complicated if we had:
  - Not paid attention to the residual plots.
  - Not used our subject matter knowledge to ignore loose collets!

#### Practical DOE "Tricks of the Trade"



- Using standard error to constrain optimization
- Employing C<sub>pk</sub> (or P<sub>pk</sub>) to optimize your DOE
- Combining categoric factors
- A Couple of Case Studies
  - The Loose Collet
  - A Case to Test Your Metal
     Trick to detect outlier and investigation save the day.

# A Case to Test Your Metal \* Background (page 1 of 2)





A customer of Stat-Ease examined his aluminum casting process using a fractional factorial design. He studied five factors in a 2<sup>5-1</sup> factorial design:

- A) Hot oil temperature
- B) Trip in mm
- C) Molten aluminum temperature
- D) Fast shot velocity
- E) Dwell time

The fraction defective out of 100 parts, was recorded for each design point. To his dismay, none of the factors seemed to make any difference.

<sup>\*</sup> From Stat-Ease client files: Dave DeVowe, Tool Products

## A Case to Test Your Metal \* Background (page 2 of 2)





### Look at the Response Data

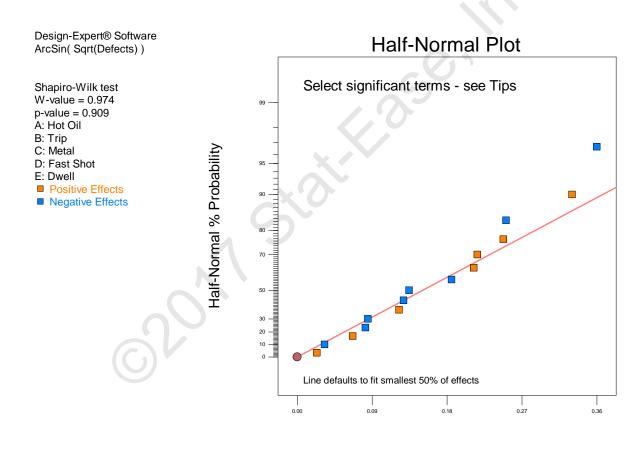
| Select | Std | Run 🗸 | Factor 1<br>A:Hot Oil<br>Degrees F | Factor 2<br>B:Trip<br>mm | Factor 3<br>C:Metal<br>Degrees F | Factor 4<br>D:Fast Shot<br>mm | Factor 5<br>E:Dwell<br>sec | Response 1<br>Defects<br>Fraction |
|--------|-----|-------|------------------------------------|--------------------------|----------------------------------|-------------------------------|----------------------------|-----------------------------------|
|        | 13  | 1     | 350                                | 390                      | 1300                             | 2.20                          | 5.50                       | 0.30                              |
|        | 15  | 2     | 350                                | 410                      | 1300                             | 2.20                          | 3.50                       | 0.22                              |
|        | 6   | 3     | 450                                | 390                      | 1300                             | 1.60                          | 5.50                       | 0.90                              |
|        | 14  | 4     | 450                                | 390                      | 1300                             | 2.20                          | 3.50                       | 0.06                              |
|        | 11  | 5     | 350                                | 410                      | 1260                             | 2.20                          | 5.50                       | 0.38                              |
|        | 16  | 6     | 450                                | 410                      | 1300                             | 2.20                          | 5.50                       | 0.38                              |
|        | 4   | 7     | 450                                | 410                      | 1260                             | 1.60                          | 5.50                       | 0.42                              |
|        | 8   | 8     | 450                                | 410                      | 1300                             | 1.60                          | 3.50                       | 0.14                              |
|        | 1   | 9     | 350                                | 390                      | 1260                             | 1.60                          | 5.50                       | 0.14                              |
|        | 9   | 10    | 350                                | 390                      | 1260                             | 2.20                          | 3.50                       | 0.22                              |
|        | 12  | 11    | 450                                | 410                      | 1260                             | 2.20                          | 3.50                       | 0.12                              |
|        | 2   | 12    | 450                                | 390                      | 1260                             | 1.60                          | 3.50                       | 0.98                              |
|        | 7   | 13    | 350                                | 410                      | 1300                             | 1.60                          | 5.50                       | 0.28                              |
|        | 3   | 14    | 350                                | 410                      | 1260                             | 1.60                          | 3.50                       | 0.36                              |
|        | 10  | 15    | 450                                | 390                      | 1260                             | 2.20                          | 5.50                       | 0.26                              |
|        | 5   | 16    | 350                                | 390                      | 1300                             | 1.60                          | 3.50                       | 1.00                              |

Note:
Lots of variation in the response!

## A Case to Test Your Metal Analysis – First Pass



#### Notice all the effects fall in a line!



|Standardized Effect|

## A Case to Test Your Metal Analysis – Second Pass



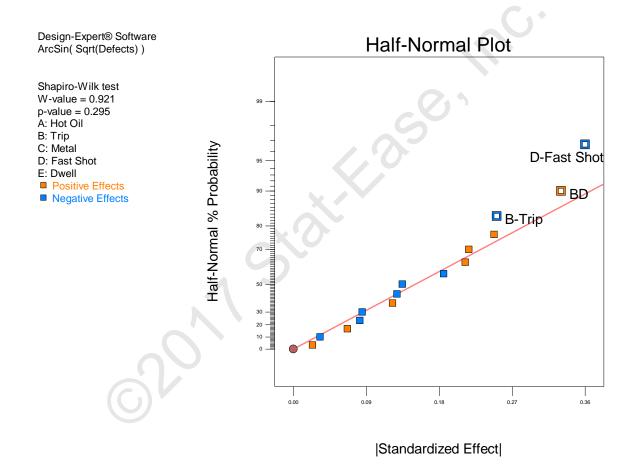
Lots of variation in the responses, but no effects!

Procedure to detect a possible outlier:

- 1. Pick a couple of the most extreme effects on the half normal plot.
- 2. Look for a potential outlier.
- 3. Judge influence of potential outlier.
- 4. Investigate the suspected outlier.
- 5. "Ignore" the outlier and reanalyze the design.

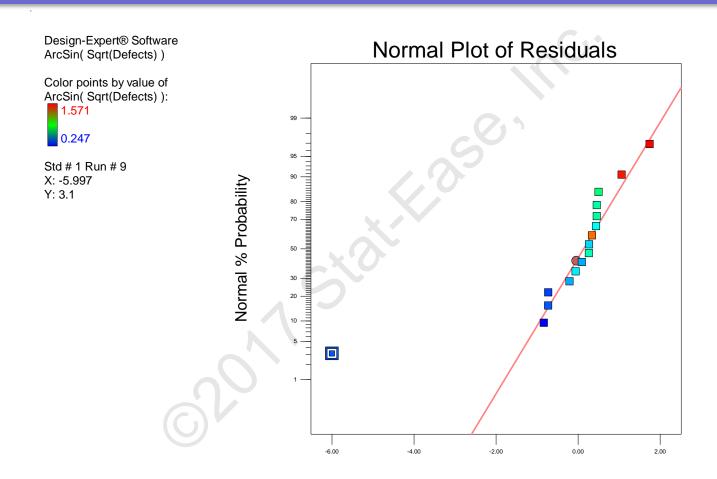
## 1. Pick a couple of the most extreme effects on the half normal plot.







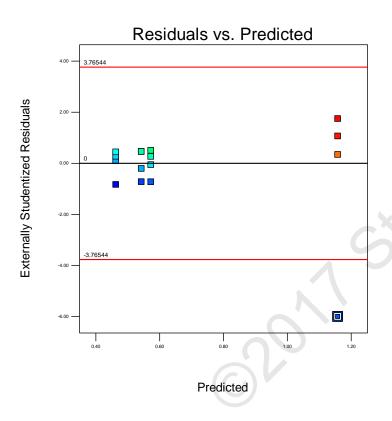


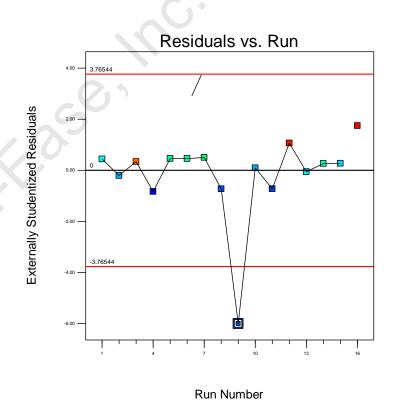


**Externally Studentized Residuals** 



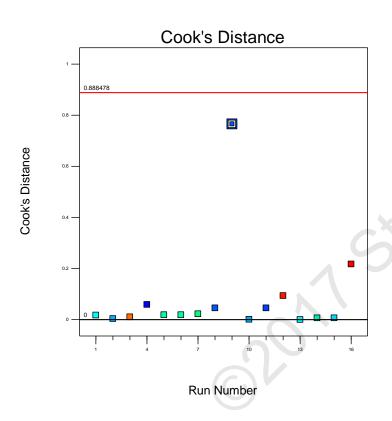


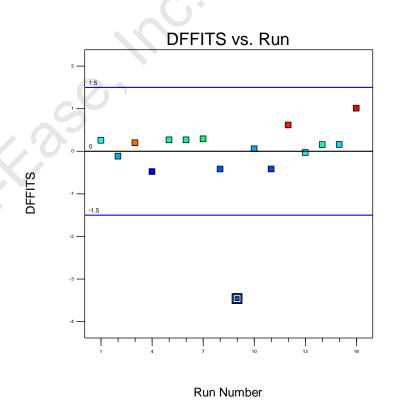




### 3. Judge influence of potential outlier.



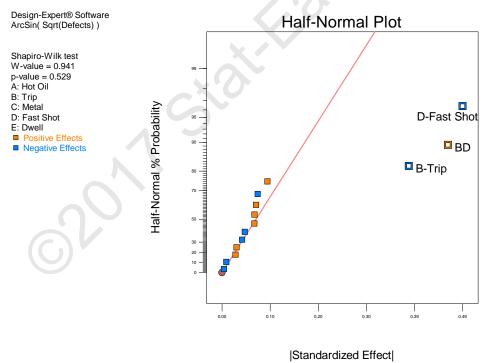






- 4. Investigate the suspected outlier.

  (The operator confirmed problems with run 9 (std 1))
- 5. "Ignore" the outlier and reanalyze the design.



## A Case to Test Your Metal Analysis – Second Pass



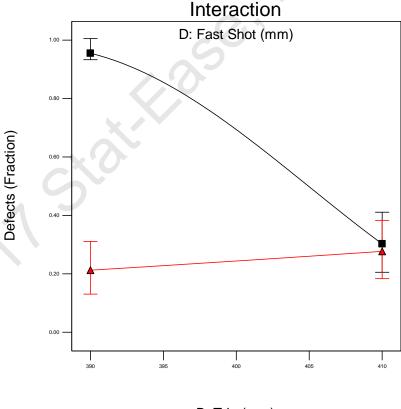
### Do not use a 390 "Trip" with a 1.60 "Fast Shot":

Design-Expert® Software Factor Coding: Actual Original Scale Defects (Fraction)

X1 = B: Trip X2 = D: Fast Shot

Actual Factors
A: Hot Oil = 400
C: Metal = 1280
E: Dwell = 4.50

■ D- 1.60 ▲ D+ 2.20



B: Trip (mm)

#### References

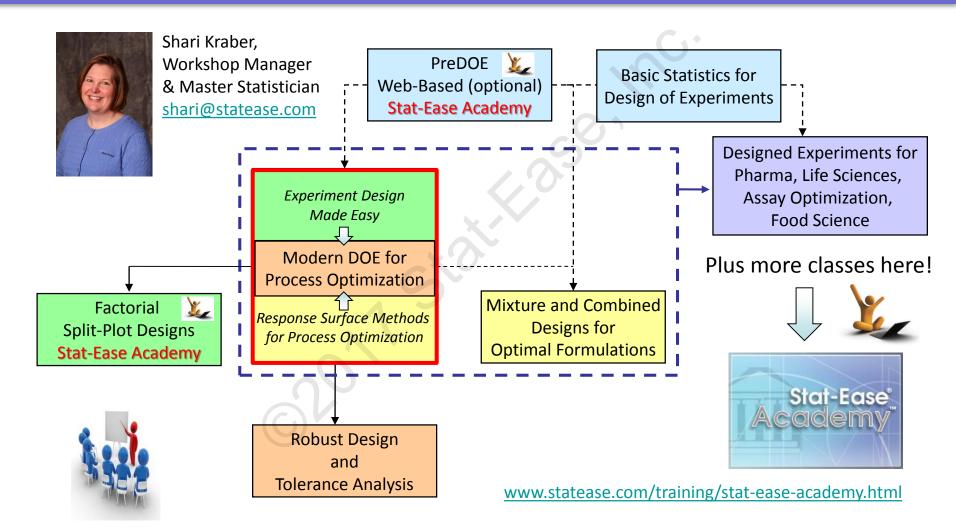


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- 6. Mark J. Anderson and Patrick J. Whitcomb (2005), RSM Simplified Optimizing Processes Using Response Surface Methods for Design of Experiments, Productivity, Inc.
- 7. Raymond H. Myers, Douglas C. Montgomery and Christine M. Anderson-Cook (2009), 3<sup>rd</sup> edition, *Response Surface Methodology*, John Wiley and Sons, Inc.

## Stat-Ease Training:

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## **Practical DOE – "Tricks of the Trade"**

Reminder, this presentation is posted at:

www.statease.com/training/webinar.html

If you have additional questions email them to:

pat@statease.com

Thank you for joining me today!